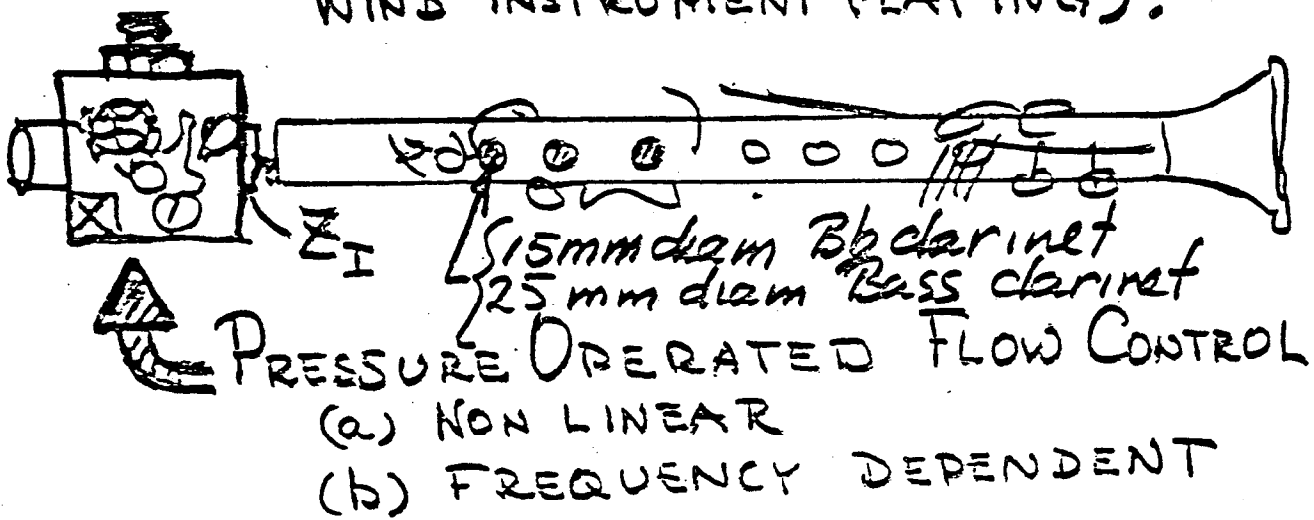
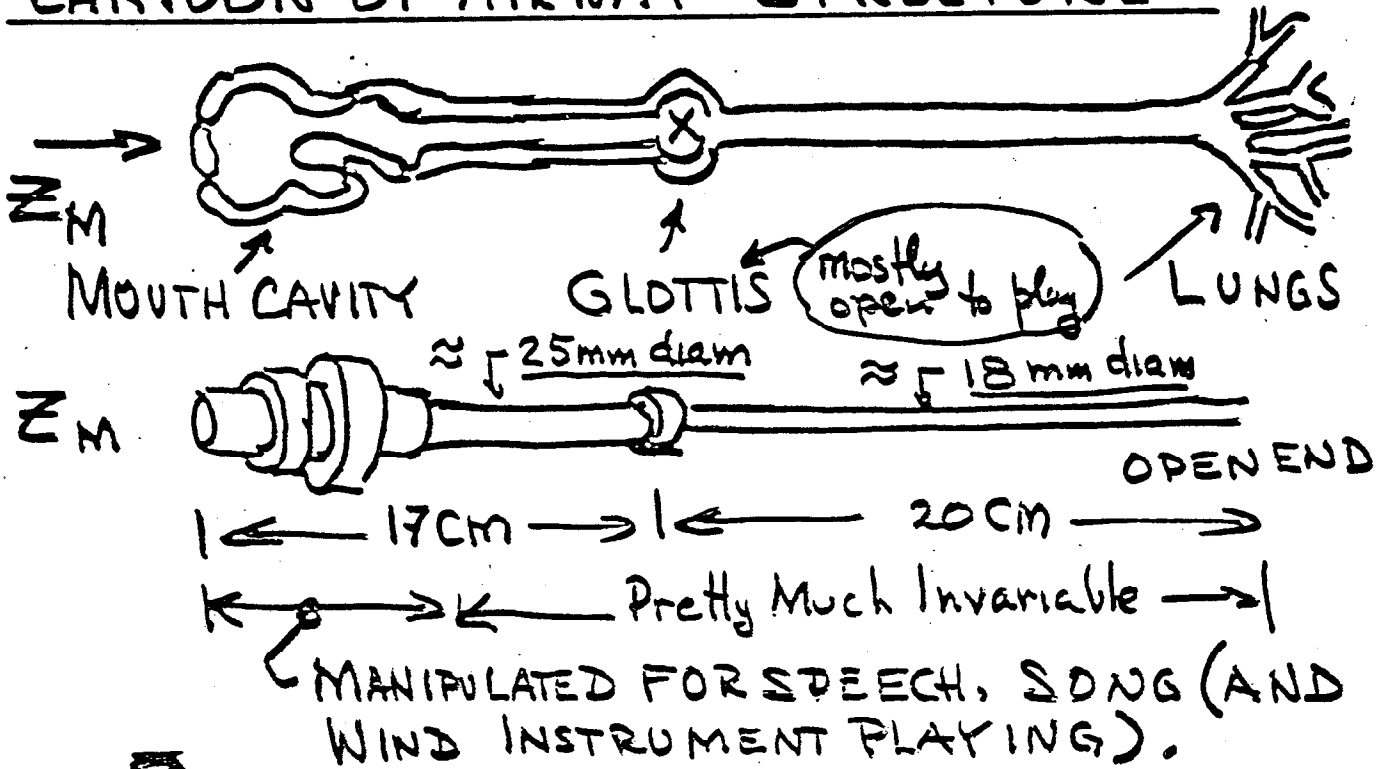


Vocal tract effects in wind instrument regeneration. A. H. Benade and P. L. Hoekje (Department of Physics, Case Western Reserve University, Cleveland, OH 44106)

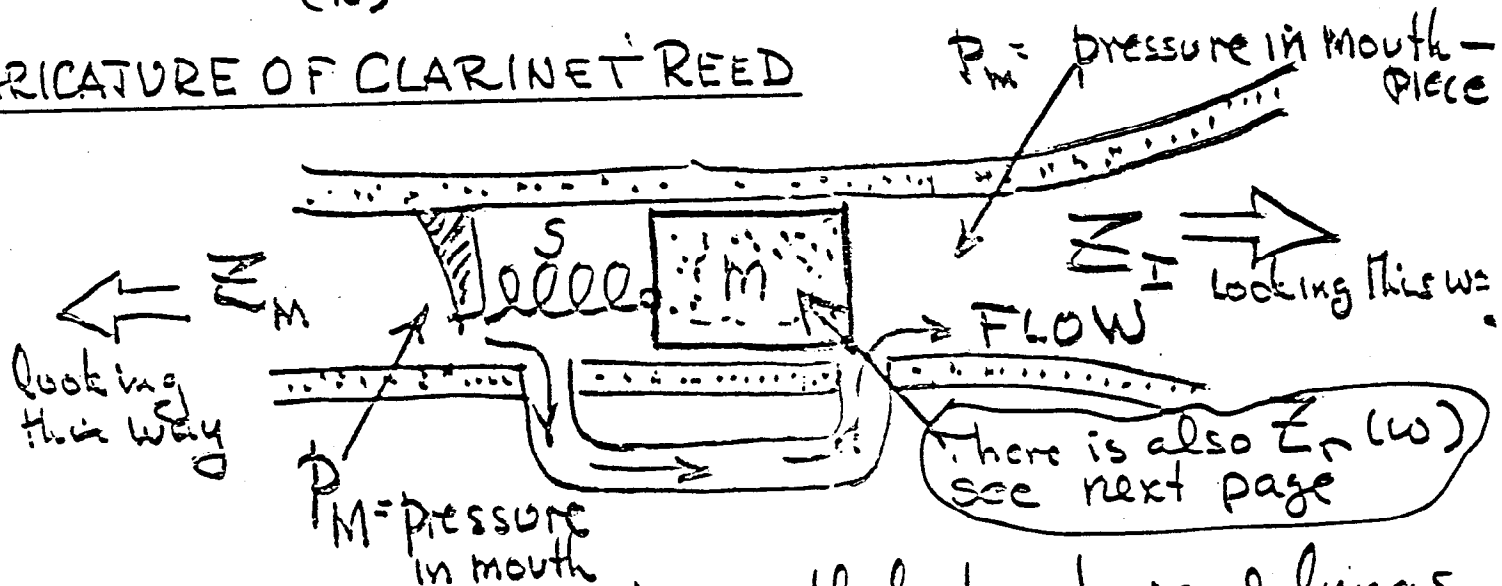
Wind players are much concerned with vocal tract influences on tone production. Laboratory study has been inconclusive, in part from inadequate theoretical formulation. A reed valve is opened and closed by the pressure difference ($p_m - p_M$) across it: p_m in the instrument's mouthpiece, p_M in the player's mouth. The reed transconductance $A = \partial u / \partial (p_m - p_M)$ depends on its natural frequency ω_r and its damping, becoming large near ω_r . The condition for oscillation is $A[(Z_m + Z_M) / Z_r] \geq 1$. We note that the reed impedance Z_r is paralleled by the sum of Z_m and Z_M . Oscillation requires $\text{Im}(Z_m + Z_M) \neq 0$, with sign depending on the low-frequency sign of A (positive for woodwinds, negative for brasses); whence woodwinds play with $\omega \leq \omega_r$, brasses with $\omega \geq \omega_r$. These results extend to large amplitude (mode-coupled) regimes of oscillation in the familiar way. Available data show resonance bandwidths of Z_M are much larger than those of Z_m (with smaller magnitude fluctuations), explaining the difficulty of direct measurement of musical effects. During tonal startup on long instruments (e.g., horn, tuba), Z_m changes as successive reflections build up the standing wave. By itself Z_m does not generally satisfy the regeneration condition during onset, thus giving a crucial role to the vocal tract. Results of experiments in progress will be presented. [Work supported by NSF.]

JASA 71:591 (1982)

CARTOON OF AIRWAY STRUCTURE



CARICATURE OF CLARINET REED



$Z_M(\omega)$ Measured in player's mouth looking toward lungs

$Z_m(\omega)$ Measured as mouthpiece looking down the INSTRUMENT

RECAPITULATE AND CONTINUE

Z_M = player's airway input impedance as seen by the reed (New stuff)

Z_I = instrument's input impedance as seen by the reed (Old Family)

Z_r = Reed's own impedance = $\frac{\text{(net driving pressure)}}{\text{(displaced air flow rate)}}$
(Since Weber, Bouasse) \rightarrow (Since Benede)

A_r = Transconductance of reed as a flow controller = flow/activating pressure diff

A VERY SMALL EXTENSION OF THE FAMILIAR RESULTS OF (Weber, Helmholz, Bouasse, Benede, Backus, Norman, Schumacher, Fletcher, Thompson.....)

SHOWS THAT IN LINEAR LIMIT

$$(1/A_r) = Z_r // (Z_I + Z_M) \xrightarrow{\text{Simply}} \text{Replace } Z_I \text{ by } (Z_I + Z_M)$$

HERE IT IS!

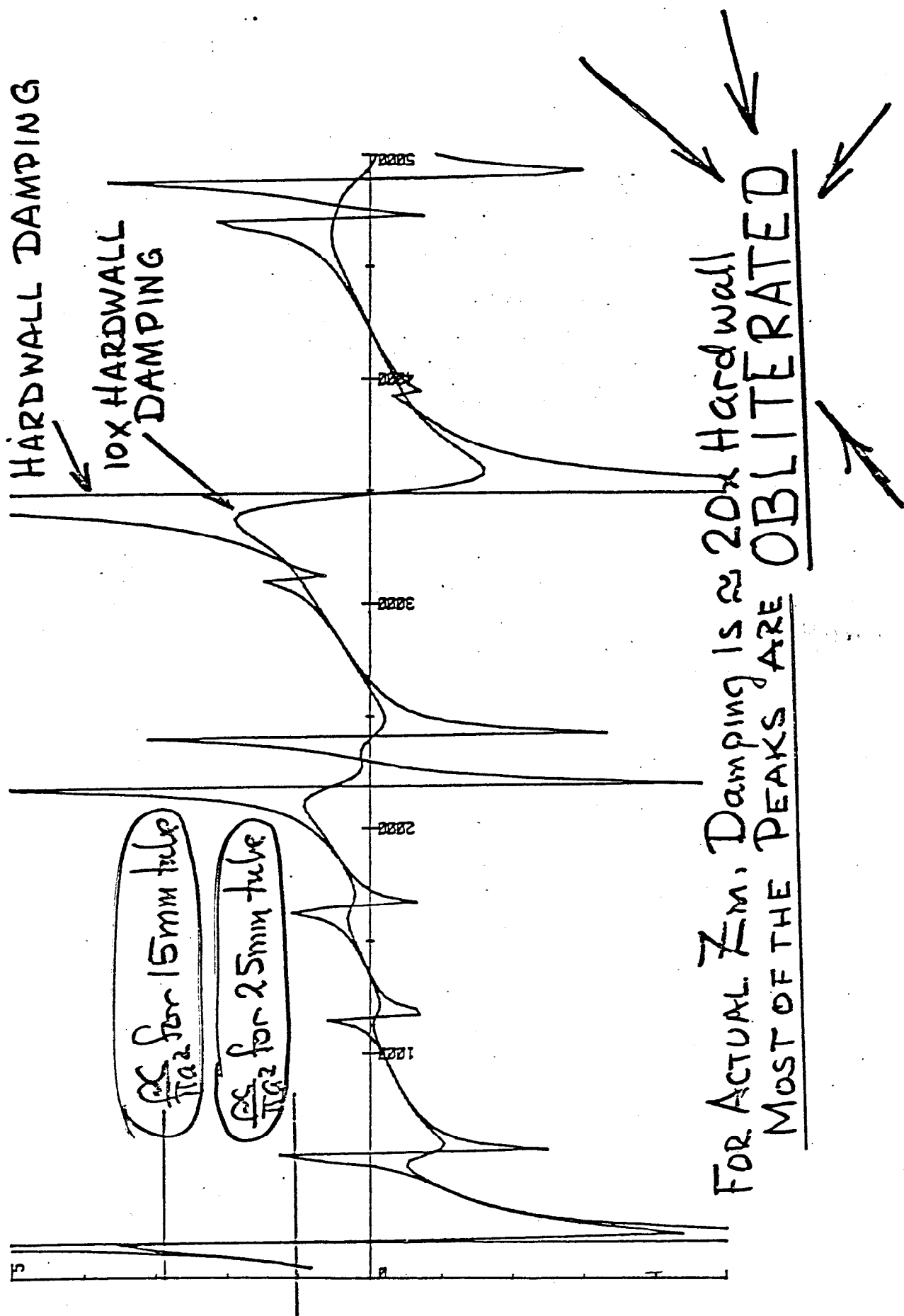
AT HIGHER PLAYING LEVELS... REGIMES OF OSCILLATION EXACTLY AS BEFORE

SIMPLY REPLACE AIR COLUMN Z ($\equiv Z_I$)

ONCE AGAIN BY SUM OF AIR COLUMN Z_A AND $\{$ PLAYERS AIRWAY Z_M

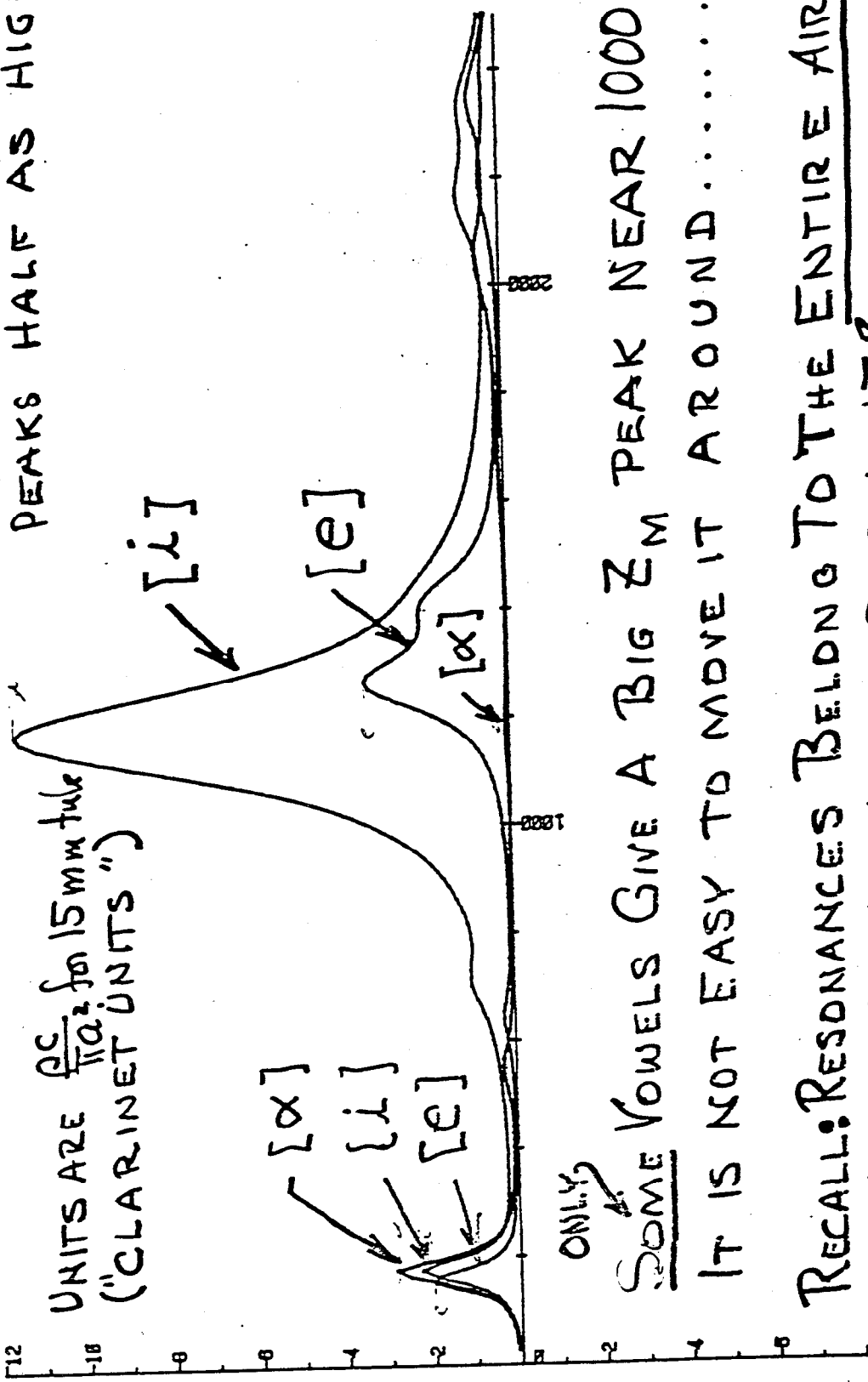
Why then has Z_M not muddled or muddled our consciousness \rightarrow ell now ?/??

CALCULATED Z_M FOR UPPER TRACT CONFIGURATION
 CORRESPONDING TO VOWEL [a:] (FANT'S DATA)
 Shows Z_M ONLY!



REAL PART OF Z_M FOR THREE VOWEL CONFIGURATIONS (DAMPING 10X HARDWALL)

REAL SYSTEM 20X, SO
PEAKS HALF AS HIGH



ONLY
SOME VOWELS GIVE A BIG Z_M PEAK NEAR 1000 Hz
IT IS NOT EASY TO MOVE IT AROUND.....

RECALL: RESONANCES BELONG TO THE ENTIRE AIRWAY
NOT TO ANY SUB-SEGMENT!

Exceptions to this are exceedingly rare

Z_M PEAK ON TOP OF

Z_I PEAK

$$\left(\frac{RC}{\pi \omega L}\right)_M = \left(\frac{1}{Q}\right) \left(\frac{RC}{\pi \omega L}\right)_I$$

$$Q_M = \left(\frac{1}{Q}\right) Q_I$$

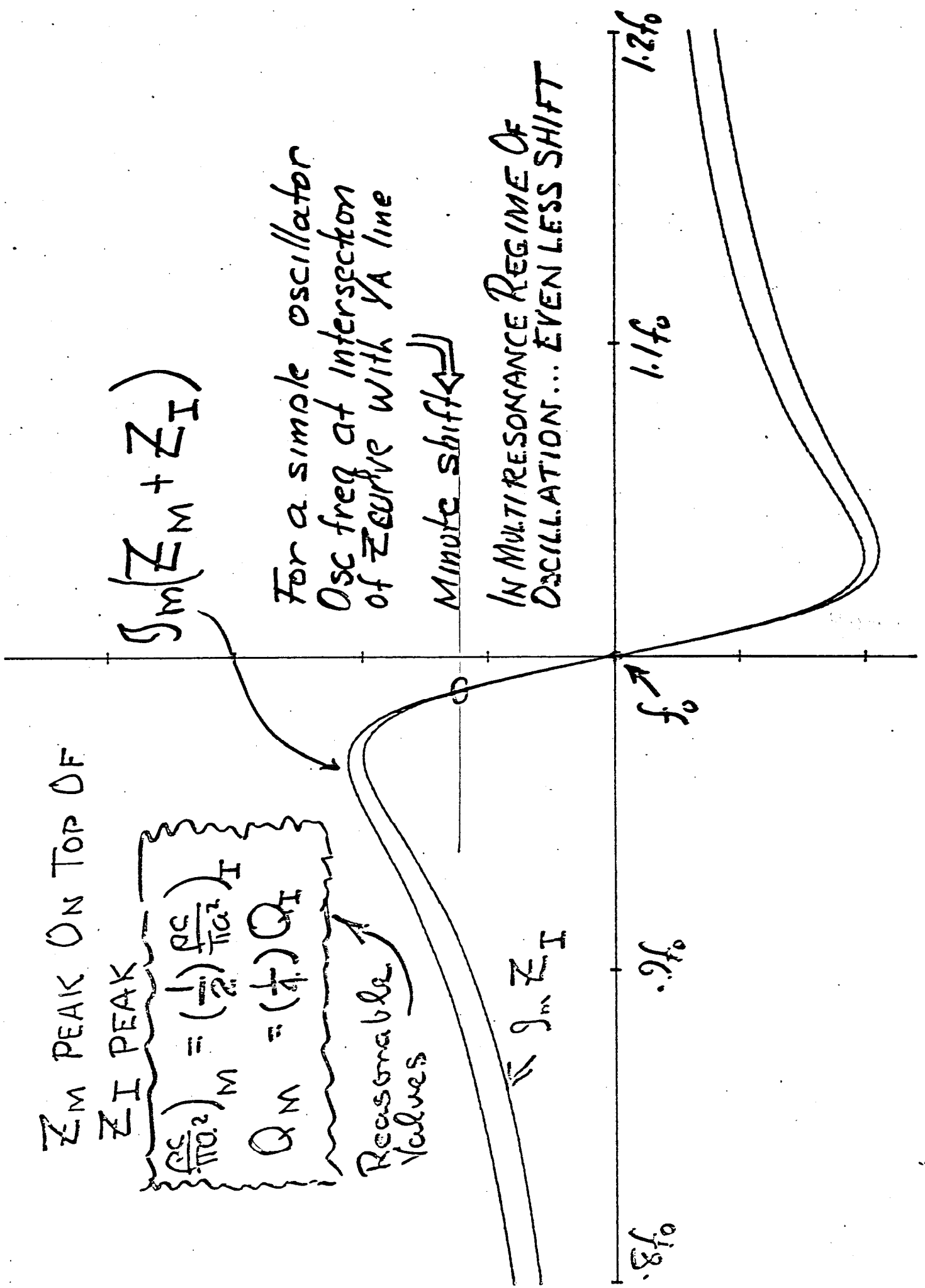
Reasonable Values

$$S_M(Z_M + Z_I)$$

For a simple oscillator
Osc freq at intersection
of Z curve with Y_A line

Minute shift \leftarrow

IN MULTIRESONANCE REGIME OF
OSCILLATION... EVEN LESS SHIFT



$0.8f_0$

$0.9f_0$

f_0

$1.1f_0$

$1.2f_0$

$\approx S_M Z_I$

7

Z_M PEAK AT FREQUENCY ≈ 0.9 FREQUENCY OF Z_I PEAK (f_0)

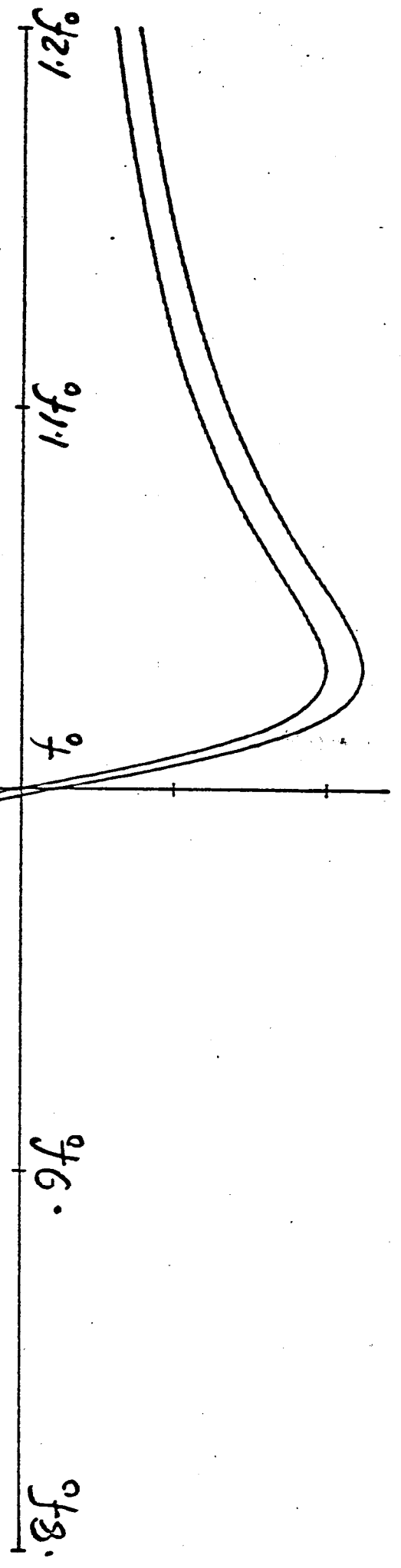
$$Q_M = \left(\frac{1}{4}\right) \frac{Q_C}{\pi C^2} I$$

$$Q_M = \left(\frac{1}{4}\right) Q_I$$

$$g_m (Z_M + Z_I)$$

$$g_m Z_I$$

Very small shift of playing frequency for a simple oscillator

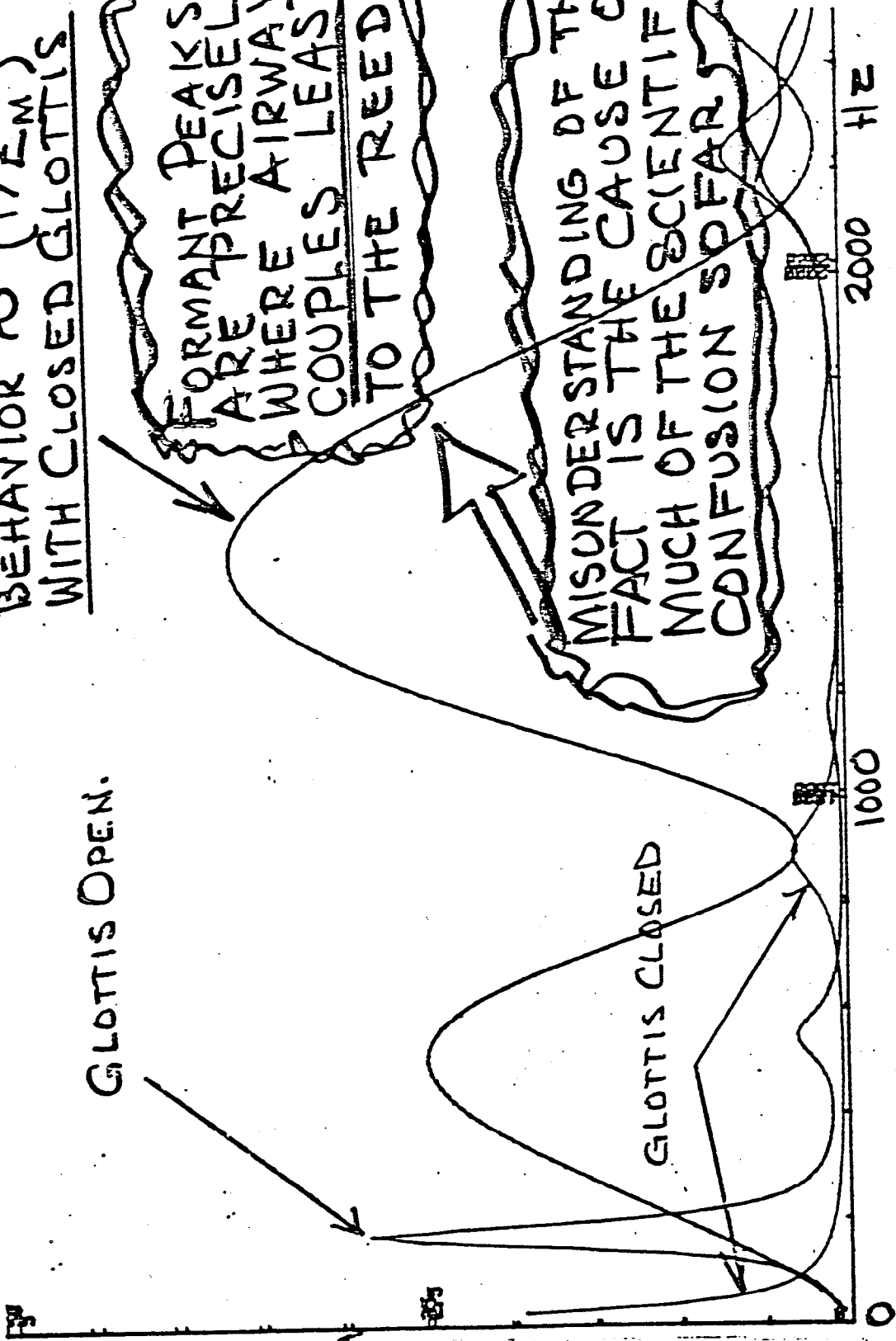


VOWEL CONFIGURATION FOR [α] 10x HARDWALL DAMPING
(REAL AIRWAY 20x HARDWALL)

ORDINARY FORMANT BEHAVIOR $\sim (1/Z_M)$ WITH CLOSED GLOTTIS

FORMANT PEAKS ARE PRECISELY WHERE AIRWAY COUPLES LEAST TO THE REED

MISUNDERSTANDING OF THIS FACT IS THE CAUSE OF MUCH OF THE SCIENTIFIC CONFUSION SO FAR



FREQUENCY →

HOW CAN WE CHECK ALL THIS???

1 Marshall a great deal of practical examples from the world of players.
Check Z_I RELATIVE TO Z_M

OVER THE PLAYING RANGE

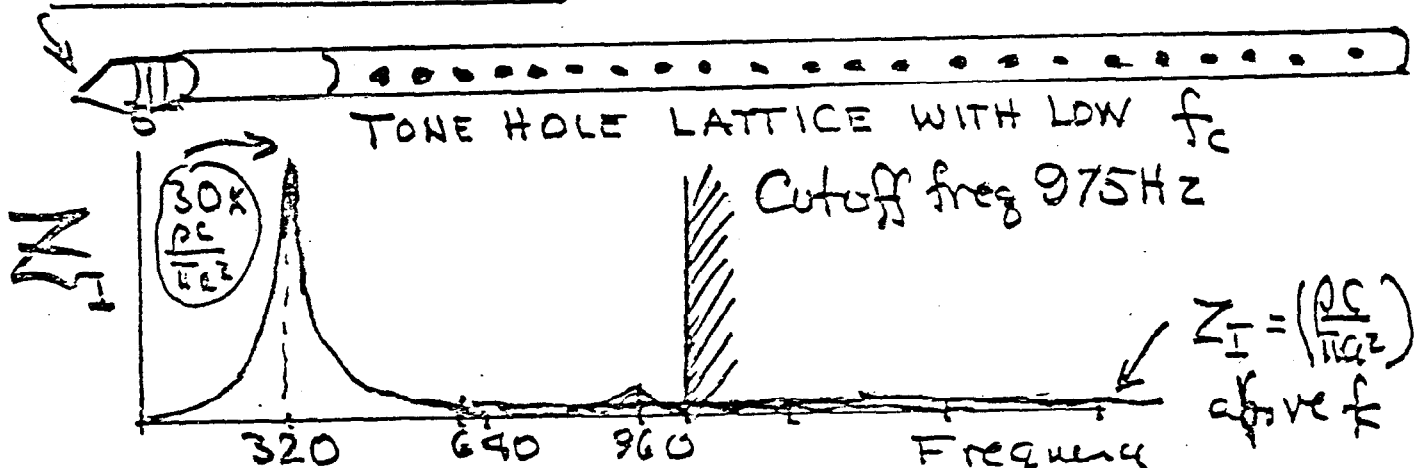
FOR EXAMPLE Bb clarinet diam $\approx 15\text{mm}$
Bass cl diam $\approx 25\text{mm}$
Contra bass diam $\approx 35\text{mm}$

Mouth and supra-glottal region avg-diam 25mm Bass is Specialist's instrument

2 Try informal playing experiments moving vocal tract to traverse configuration with 1000 Hz peak. Select notes to play that have components near 1000 Hz and look for any odd behavior in PITCH, TONE, STABILITY

3 Devise Air Column with SIMPLE, FAMILIAR ACOUSTIC PROPERTIES, that will "EXPOSE" the effects of the 1000 Hz Z_M peak.

CLARINET MOUTHPIECE



ONE TALL PEAK FOR Z_I } HARD TO PLAY
} \sim SINUSOID SIGNAL

WE HAVE TWO SPECTRA TO WORRY ABOUT
 (1) "MOUTH PIECE SPECTRUM", (2) MOUTH SPECTRUM

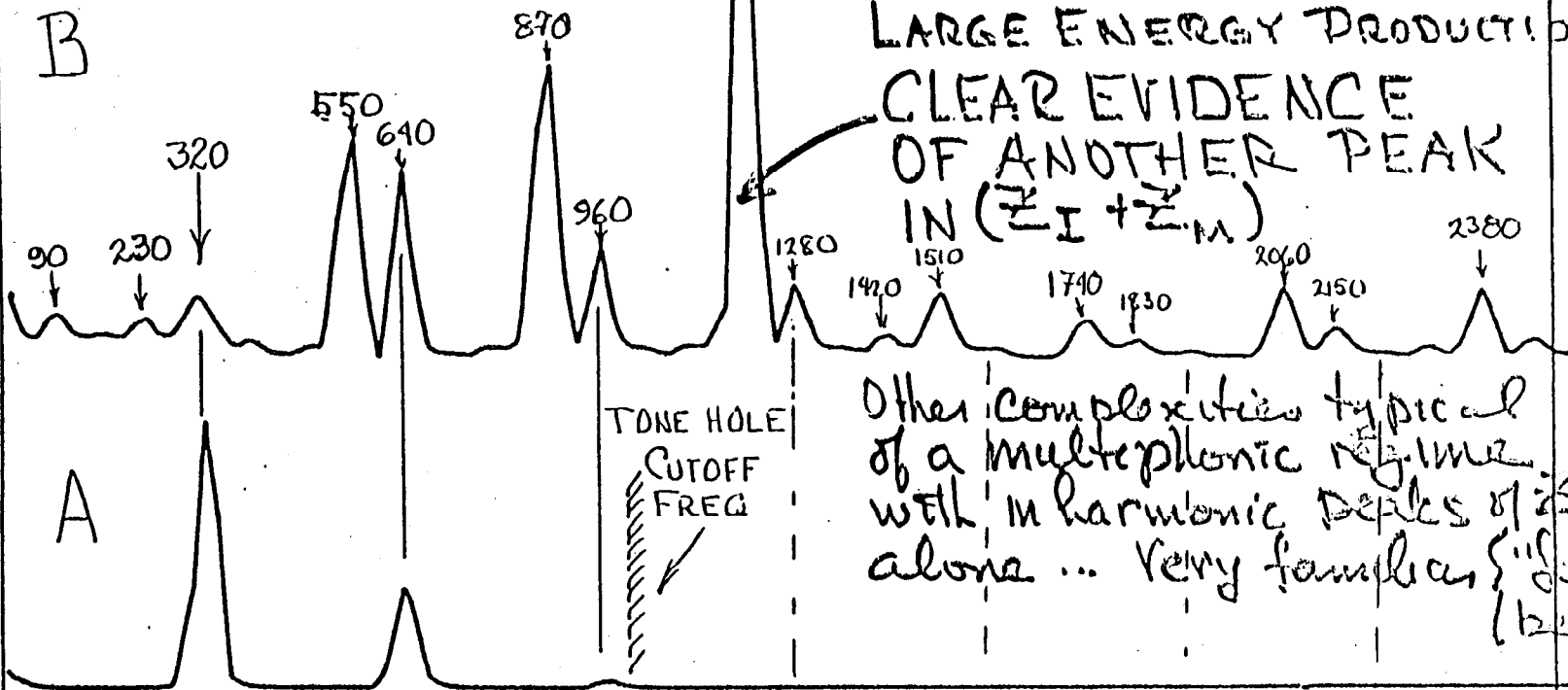
(1) $Z_I \times$ Flow Spectrum

(2) $Z_M \times$ Flow spectrum

MOUTH SPECTRUM

A. "NORMAL"

B. MULTIPHONIC VIA TONGUE POSITION



LARGE ENERGY PRODUCTION HAS
 CLEAR EVIDENCE
 OF ANOTHER PEAK
 IN ($Z_I + Z_M$)

Other complexities typical
 of a multiphonic regime
 with n harmonic peaks of Z_I
 alone ... very familiar "feel" and
 behavior

DIRECT PRODUCTION VIA PEAK OF Z_I ... ($Z_I + Z_M$) negligible
 small amount of second harmonic via real non-resonance at DIP of $Z_I + Z_M$!