

PERTURBATION THEORY AND ITS
APPLICATION TO MUSICAL AIR
COLUMN ADJUSTMENT
A. H. BENADE

LECTURE FOR NORDA AT NATIONAL SPACE TECHNOLOGY LABS,
BAY ST. LOUIS, MISSISSIPPI - DEPT OF THE NAVY

10 JANUARY 1985

WHAT IS THE WAVE EQUATION?

As long as density & bulk modulus are same everywhere
Rayleigh 1876 etc etc

$$\begin{cases} \phi(x,r) = \int_0^r [\sqrt{\frac{\partial^2}{\partial x^2} + (\omega/c)^2}] F(x) \\ F(x) = \phi(x,0) \end{cases}$$

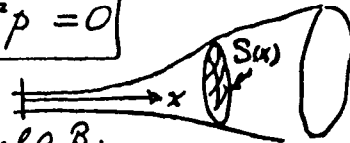
With shape of boundaries coming in via

$$-\frac{\partial \phi}{\partial x} \frac{\partial a}{\partial x} + \frac{\partial \phi}{\partial r} = 0 \quad r=a \text{ at wall}$$

Simplified version known for 200 years is

$$p'' + (S'/S)p' + k^2 p = 0$$

Note that Z depends
on shape of horn, and on local ρ, B .



This is not too hard to solve, not too hard to "understand"
has many interesting kinds of systematic behavior

"TEXTBOOK PERTURBATION THEORY" (as in QM)

$$\Delta \omega_n = \frac{\text{const}}{\omega_n} \int S_0(x) p_n''(x) \tilde{p}_n''(x) dx$$

$$\int \left[\frac{e'}{a_0} + \frac{e}{a_0} \frac{2a_0'}{a_0} \right]$$

THIS IS A MESS TO THINK WITH

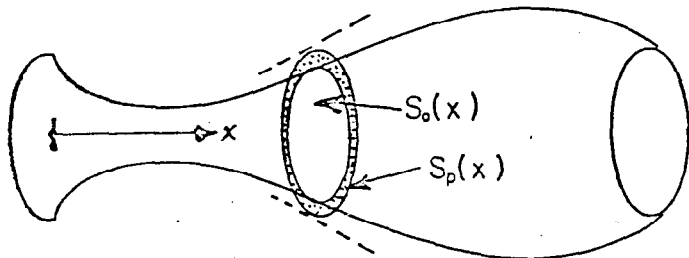
IT ISN'T EVEN RIGHT UNLESS YOU CAN PROPERLY
SHOW THE ORTHOGONALITY OF THE p_n 's.

(Trouble arises from boundary conditions at ends where
one usually gets $(P/p)' = (\text{function of } \omega) !$)

There are many nicer ways to
get $\Delta \omega_n$... that don't depend
on orthog. p_n 's

①

A FRIENDLY PERTURBATION METHOD



CROSS SECTION CHANGE = $S_p(x)$

EHRENFE ST'S ADIABATIC INVARIANCE

ΔE = WORK DONE AGAINST RADIATION
PRESSURE AS WALLS ARE MOVED
TO GIVE HORN NEW SHAPE

RADIATION PRESSURE = $U(x) - K(x)$
 U, K = PE, KE DENSITIES

$$\begin{aligned} (\Delta\omega/\omega)_n &= \frac{\int [K(x) - U(x)]_n S_p(x) dx}{\int [K(x) + U(x)]_n S_0(x) dx} \\ &= \frac{\int [\text{LAGRANGIAN DENSITY}] S_p dx}{\int [\text{ENERGY DENSITY}] S_0 dx} \end{aligned}$$

$$U_n(x) = (1/2B)p_n^2(x)$$

$$K_n(x) = (\rho/2)v_n^2(x) = (1/2B)(c/\omega)_n^2 (\partial p/\partial x)_n^2$$

(2)

FOR PRACTICAL PURPOSES

WE FIND IT USEFUL TO DEFINE THE
PERTURBATION WEIGHT FUNCTION

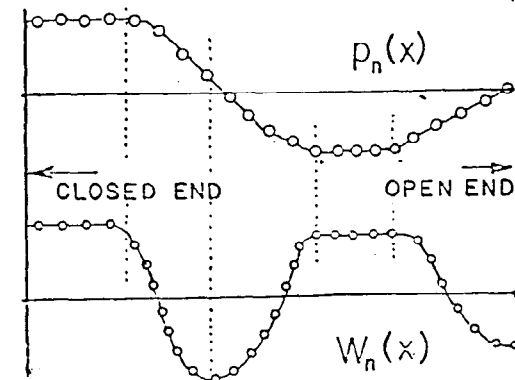
$$W_n(x)$$

SUCH THAT

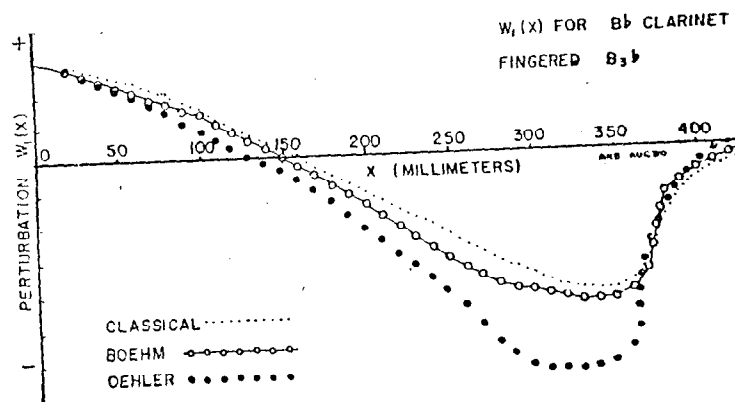
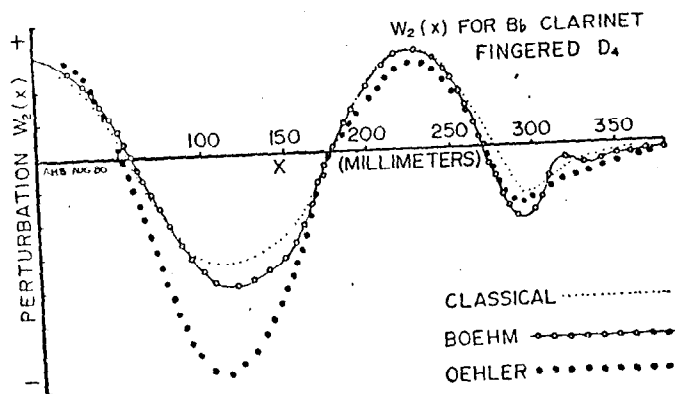
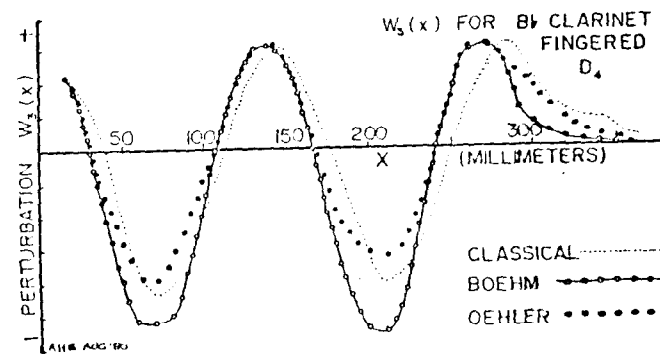
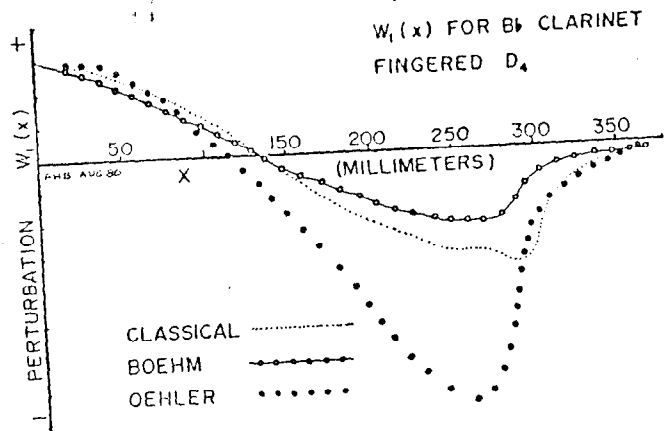
$$(\Delta F/F)_n = - \int W_n S_p dx$$

(A) ENLARGEMENT WHERE $p_n(x)$ IS
LARGE — LOWERS F_n

(B) ENLARGEMENT WHERE GRAD p
IS LARGE — RAISES F_n

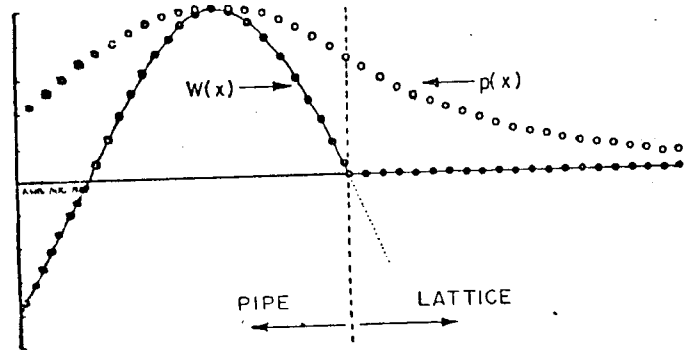
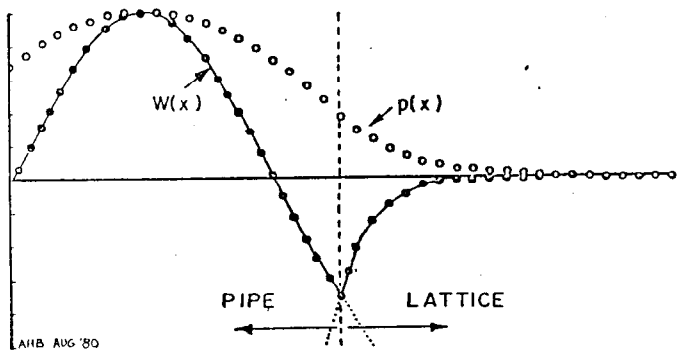
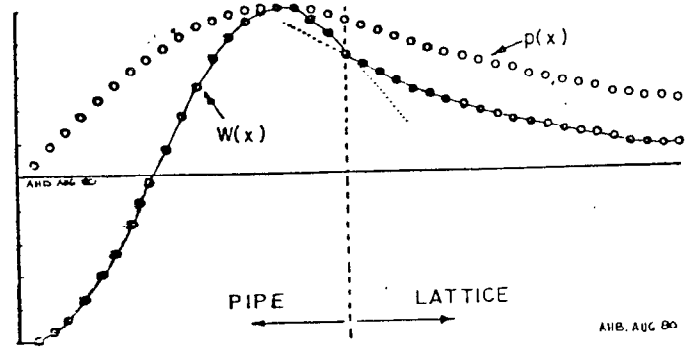
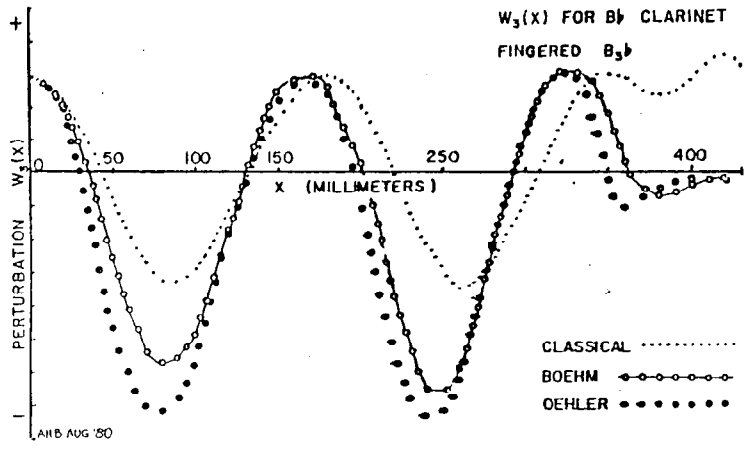


(3)



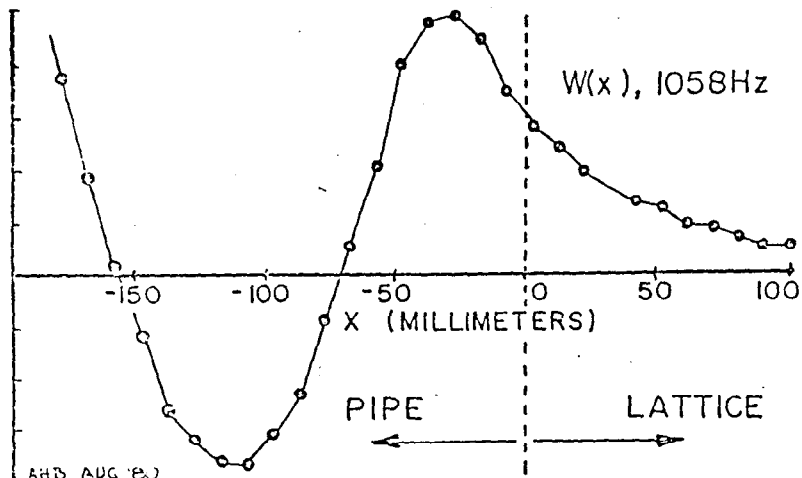
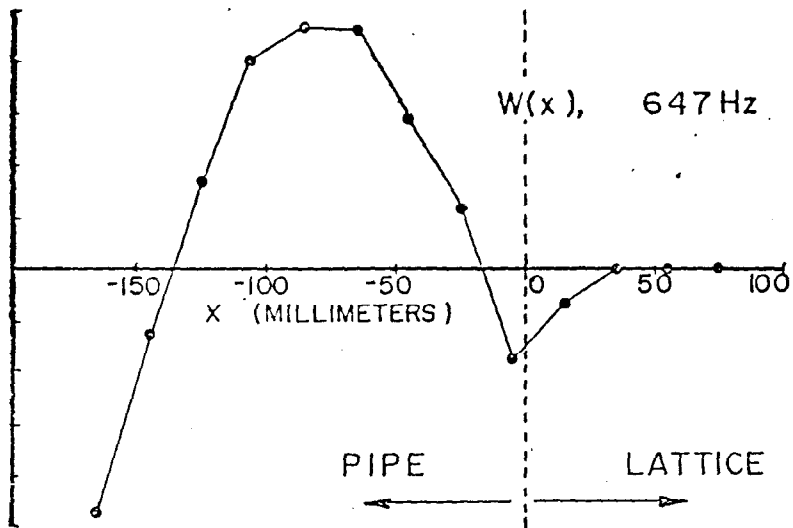
(4)

(5)



(6)

(7)

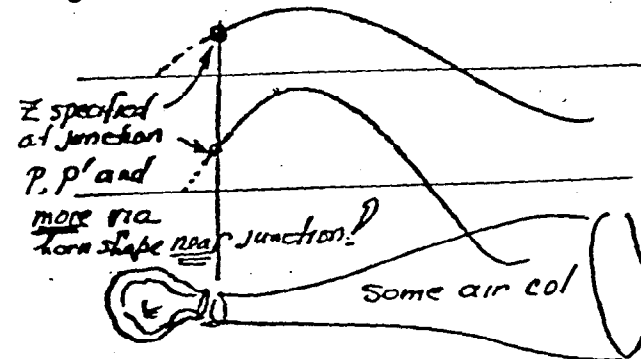


(8)

OTHER PERTURBATIONS:

(I)

Tinkering with the end conditions alters the eigen values.



This can cause endless confusion if one forgets it.

Simplest version is similar to lowering of energy levels in a potential well with walls of finite height



Note however, that these end-modifications not only stretch and shrink P_n in the main air column, they also can slide it lengthwise along it

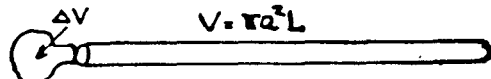
For this reason, End perts — also middle bore perts

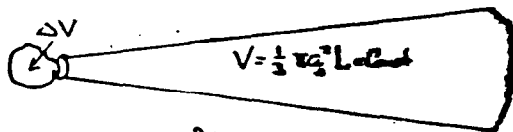
(II)

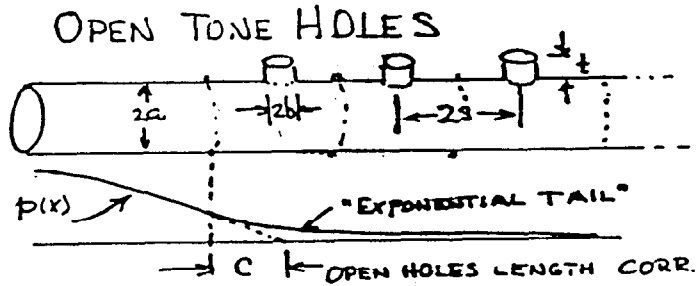
Temperature, humidity, composition gradients, viscous, thermal boundary layers, turbulence effects etc etc. **COMPLEX EIGENVALUES** → ALTERS PERT NEAR NODES OF PRESSURE, AND OF FLOW.

(9)

MOUTHPIECE AND REED CAVITY

①  $V = \pi a^2 L$
 $\left(\frac{\Delta f}{f}\right) \approx -\frac{\Delta V}{V}$ INDEP OF η

②  $V = \frac{1}{3} \pi a^2 L \frac{b^2}{a^2}$
 $\left(\frac{\Delta f}{f}\right) \approx -\left(\frac{\Delta V}{V}\right) (\text{CONST}) \cdot \eta^2$
 RISES RAPIDLY WITH η



$$C \approx s \sqrt{1 + 2 \left(\frac{t}{s}\right) \left(\frac{a}{b}\right)^2} \quad \text{FOR } f_c \ll f_c$$

$$f_c = \left(\frac{c}{2\pi}\right) \left(\frac{b}{a}\right) \sqrt{\frac{1}{2} s t}$$

