Recent CCRMA Research in Digital Audio Synthesis, Processing, and Effects

Julius O. Smith III CCRMA, Stanford University

DAFx-09, Keynote III, Como, Italy

September 4, 2009





Spring Reverb Models

Virtual Analog Circuits

Acoustic Guitar Models

Haptic Instruments

New Oscillators

Spectral Delay Filters

Audio FFT Filter Banks

Microphone Array

Faust to Flash Plugins

Summary

Overview





- Previously at DAFx06
- Research Update
- CCRMA

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Three Years Ago

In my DAFx06 review, we looked at

- Early digital audio effects (delay lines, scanner vibrato, ...)
- Acoustic propagation models
- Digital waveguide models (voice, strings, woodwinds, . . .)
- Commuted synthesis (acoustic guitar, harpsichord, piano, . . .)
- All my best accumulated sound examples!
- That presentation is available online:

http://ccrma.stanford.edu/~jos/pdf/DAFx06KeynoteII.pdf (sound examples via HTTP)

What can I talk about now?





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Since Three Years Ago

Problem:

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Solution:

Summarize recent DAFx-related research at CCRMA as a whole

Talk Design:

- New results in the past year (three years is too much)
- Developed at CCRMA
- JOS involved as collaborator or adviser
 (i.e., I know something about it!)





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DAFx-Related Research involving JOS at CCRMA, 2008-2009

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CCRMA building: The Knoll, Stanford University





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Multimodal Spring Reverb Modeling





Accutronics Type 8 Spring Tank

Overview

Spring Reverb Models

- Spring Tank
- Impulse Response
- Model
- Sound Examples

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Top: Accutronics Type 8 Spring Tank

Bot: Single Spring "Folded" into a Compact Space





Measured Single-Spring Impulse Response

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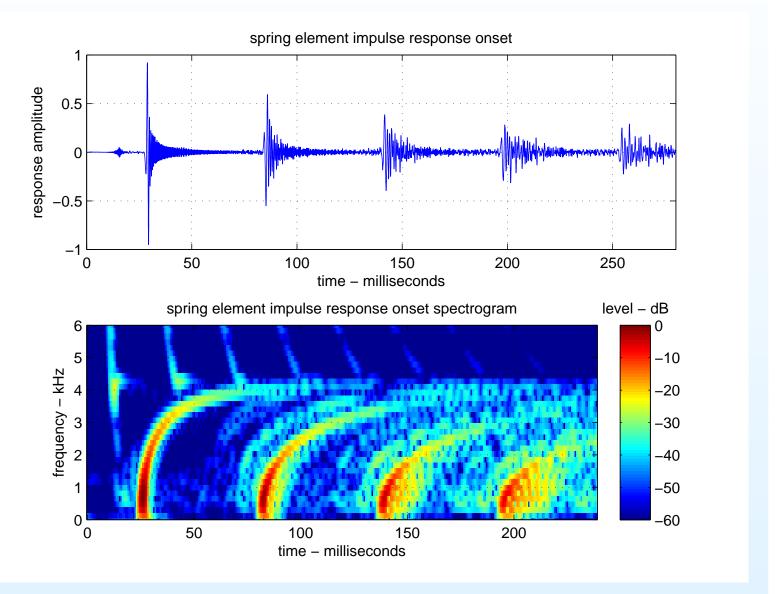
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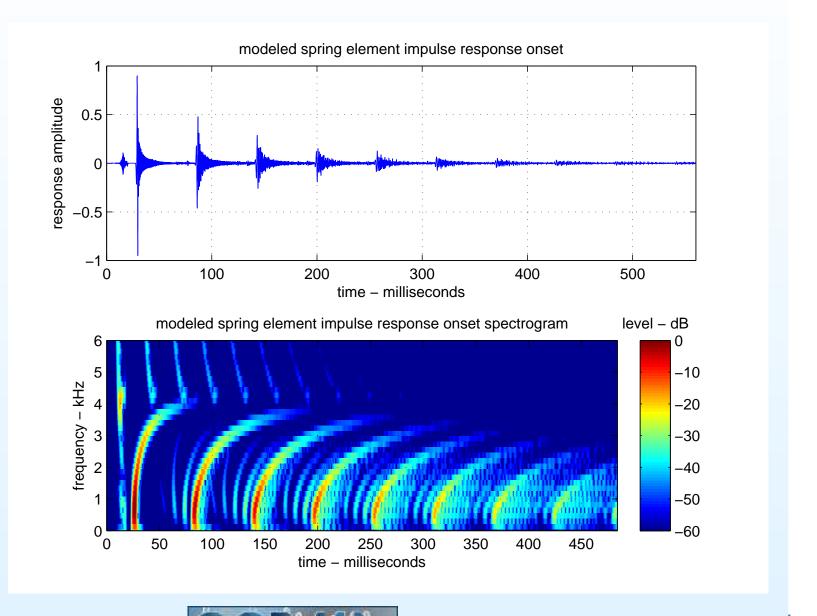
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Model Impulse Response





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Spring Reverb Sound Examples

- Dry Source Signal: (WAV) (MP3)
- Measured Spring-Reverb Response: (WAV) (MP3)
- Spring-Reverb Model Response: (WAV) (MP3)

Submitted Paper: "A Spring Reverb Model Employing Coupled Torsional and Longitudinal Modes"

Jonathan Abel, Dave Berners, Kyle Spratt, and Julius Smith

(in review)





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Digitizing Circuits in Real Time

Recent CCRMA/EE thesis by **David Yeh**:

- Analog Audio Circuits → Real-Time Digital Audio Effects
- Includes work of four past DAFx papers
- Linear and nonlinear methods for digitizing circuits
- Nonlinear methods similar to SPICE (implicit) but modified for real time circuit-solving (semi-implicit) in discrete time
- One method extends the "K Method" to
 - Nonlinear circuits, with automated application to "netlists"
 - Discrete-time nonlinear state-space formulation (resolves issues with certain circuit types)
- Instantaneous nonlinearities are "precomputed" as in K Method
- Can be applied to transistor and vacuum-tube circuits
- Accuracy limited primarily by the underlying device models





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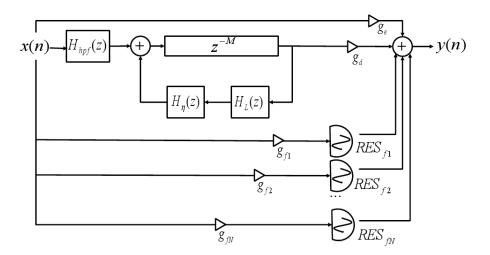
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Coupled Strings Analysis and Synthesis

Submitted paper (from pending CCRMA/CS thesis) by **Nelson Lee**:

"Analysis and Synthesis of Coupled Vibrating Strings Using a Hybrid Modal-Waveguide Synthesis Model"

Nelson Lee, Julius Smith, and Vesa Välimäki (in review)



Similar to Balázs Bank formulation, but replacing low-frequency partials by fourth-order resonators (instead of adding second-order resonators to existing partials)





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Virtual Acoustic Guitar Sound Examples of Individual Effects

From Nelson Lee's thesis defense:

- Original waveform: (WAV) (MP3)
- Simple lossless, reflectively terminated digital waveguide (DWG): (WAV) (MP3)
- Add loop filter: (WAV) (MP3)
- Add interpolation filter: (WAV) (MP3)
- Add excitation (ICMC07): (WAV) (MP3)
- Add body response: (WAV) (MP3)
- Add hybrid modal/waveguide model: (WAV) (MP3)
- Exaggerate pitch glide due to tension modulation: (WAV) (MP3)





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Virtual Acoustic Guitar Sound Examples

More Nelson Lee examples:

- Original 1: (WAV) (MP3)
- Synthesized 1: (WAV) (MP3)
- Original 2: (WAV) (MP3)
- Synthesized 2: (WAV) (MP3)
- Original 3: (WAV) (MP3)
- Synthesized 3: (WAV) (MP3)
- Original 4: (WAV) (MP3)
- Synthesized 4: (WAV) (MP3)
- Original 5: (WAV) (MP3)
- Synthesized 5: (WAV) (MP3)
- Original 6: (WAV) (MP3)
- Synthesized 6: (WAV) (MP3)
- Synthesized Chord Demo: (WAV) (MP3)





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Haptic Feedback Control for Virtual Instruments





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Haptic Virtual Musical Instruments

CCRMA/EE PhD student Ed Berdahl is working on

Haptic Feedback Control for Virtual Instruments

Dissertation expected by the end of the year

Goals:

- Assist and/or augment gestures
- Assist with accurate playing
- Recent projects:
 - Haptically plucked virtual string
 - Active drumhead (one-handed rolls, etc.):
 http://ccrma.stanford.edu/~eberdahl/Projects/ HapticDrum/





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New Digital Oscillator Algorithms





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New Oscillators

- Sawtooth Synth
- Diff'd Polynomials
- Aliasing Suppression
- More Examples
- Comparisons
- Comparisons LogF
- Aliasing Masked
- Sound Example

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Summary

Sawtooth Waveforms via Differentiated Polynomials

Given

$$f(x) = x^{n} + a_{n-1}x^{n-1} + \dots + a_{1}x + a_{0}$$

then differentiating n-1 times gives

$$f^{(n)}(x) = n! x + (n-1)! a_{n-1}.$$

This first-order polynomial (a line segment) generates a *sawtooth* waveform as x periodically traverses [-1,1].





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Differentiated Polynomial Wave (DPW) Sawtooth Synthesis

1. Digitally synthesize

$$x(n) = f\left[2\left(\frac{nT}{P} \bmod 1\right) - 1\right],$$

where

$$f(x) = x^n + a_{n-1}x^{n-1} + \dots + a_1x + a_0$$

T = sampling interval (sec)

P = desired period (sec)

n = sample number (integer)

2. Apply n-1 first-order finite differences $x_{k+1}(n) = [x_k(n) - x_k(n-1)]/(2T/P)$ to get

$$X_{n-1}(z) = \left(\frac{1-z^{-1}}{2T/P}\right)^{n-1} X(z)$$





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Minimizing Aliasing

Initial waveform is given by sampling

$$f(x) = x^n + a_{n-1}x^{n-1} + \dots + a_1x + a_0, \quad x \in [-1, 1).$$

After n-1 derivatives, we get

$$f^{(n)}(x) = n! x + (n-1)! a_{n-1}.$$

- For zero mean, set $a_{n-1} = 0$
- The n-1 remaining degrees of freedom in f(x) can be used to maximize flatness at the transition from x=1 to x=-1
- This smoothness minimizes aliasing in the synthesized sawtooth
- We can set $a_0 = 0$ because it has no effect on smoothness
- This leaves n-2 coefficients to optimize





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First Several Maximum-Smoothness Examples

Results for polynomial orders up to n=6:

$$f_2(x) = x^2$$

$$f_3(x) = x^3 - x$$

$$f_4(x) = x^4 - 2x^2$$

$$f_5(x) = x^5 - \frac{10}{3}x^3 + \frac{7}{3}$$

$$f_6(x) = x^6 - 5x^4 + 7x^2$$

Submitted Paper: "Alias-Suppressed Oscillators based on Differentiated Polynomial Waveforms"

Vesa Välimäki, Juhan Nam, Julius Smith, and Jonathan Abel

IEEE Transactions on Acoustics, Speech, and Language Processing March 2010 (accepted for publication)





Comparison of First Four Polynomial Orders

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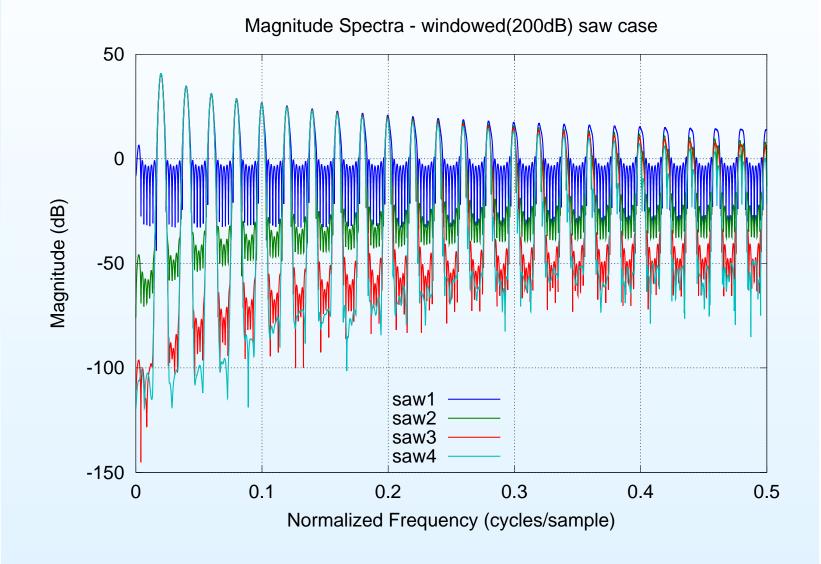
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Same Comparison over Log Frequency

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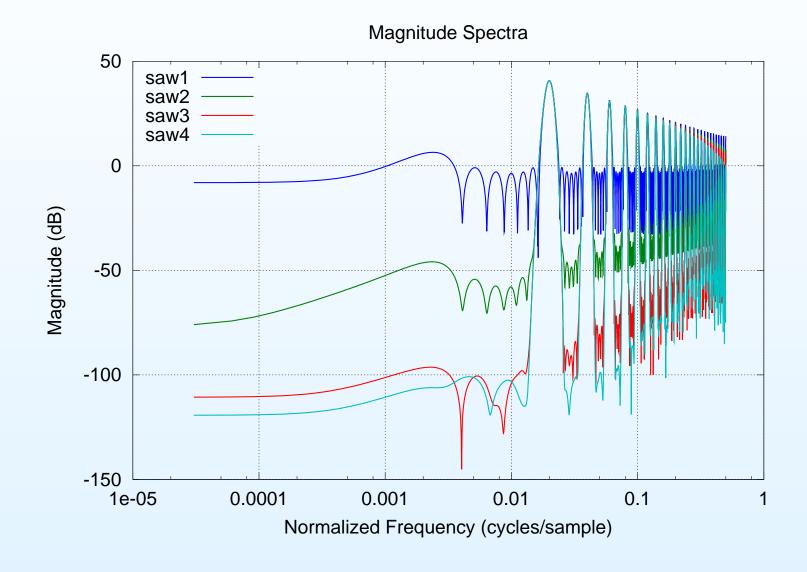
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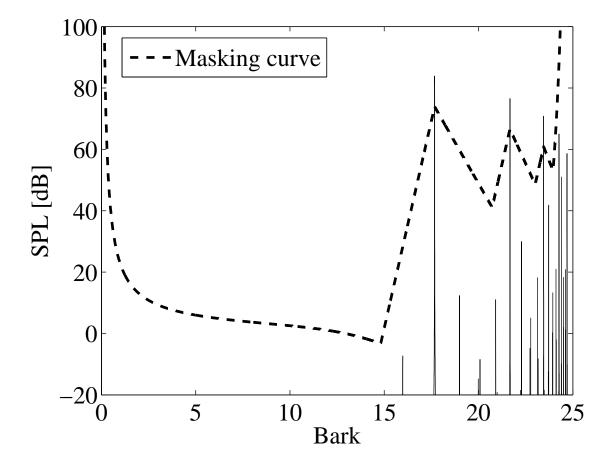
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Relation of Aliased Components to Masking Threshold



Spectrum of a sawtooth waveform over masking threshold

- F0 = 4.3 kHz, Fs = 44.1 kHz
- 3rd-order B-spline interpolation = 4th-order DPW

[Juhan Nam]





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Sound Examples

- Plain Digital Sawtooth
- Differentiated-Parabolic-Wave Sawtooth
- Doubly Differentiated Cubic-Wave Sawtooth





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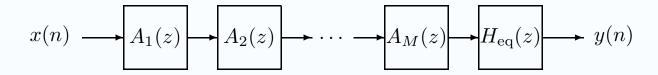
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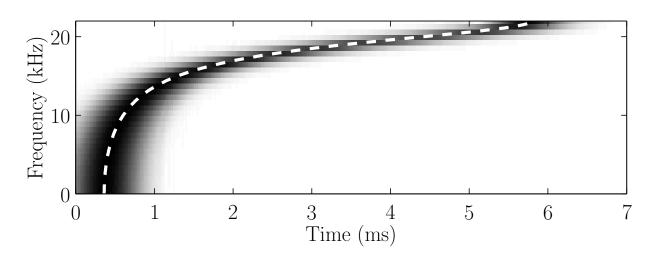
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Spectral Delay Filters





See presentation later this morning (11:20 am):

"Spectral Delay Filters with Feedback Delay and Time-Varying Coefficients"

Jussi Pekonen, Vesa Välimäki, Jonathan Abel, and Julius Smith



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Recent Paper (published online):

"Spectral Delay Filters"

Vesa Välimäki, Jonathan Abel, and Julius Smith

Journal of the Audio Engineering Society

July/August 2009





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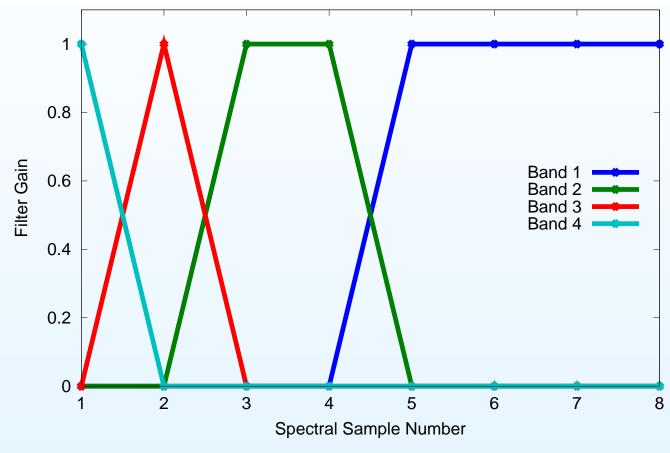
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Octave Filter Bank Schematic

Complex Octave Filter Bank



Simple octave filter bank for *complex* signals.





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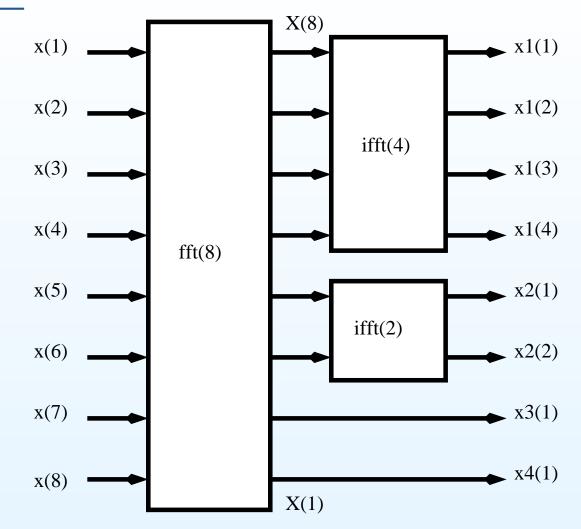
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Basic Idea



- FFT implementation of one frame of simple octave filter bank
- Successive frames non-overlapping (rectangular window)





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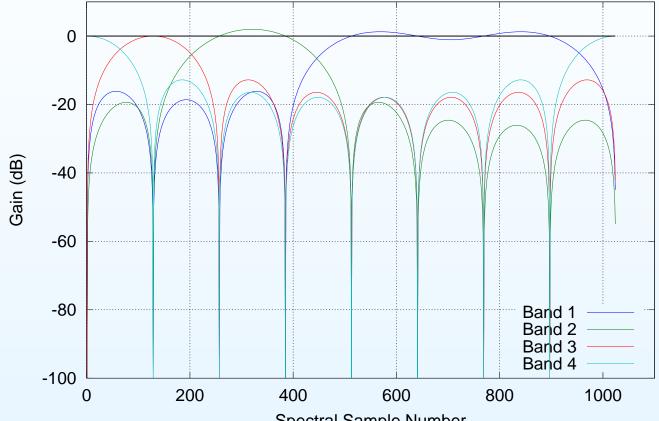
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Interpolated Frequency Response

Interpolated₁₂₈ Channel-Signal Magnitude-Spectra Overlaid



Spectral Sample Number
Channel-frequency-response overlay for three-octave filter bank

- Filter-bank driven by an impulse
- Zero-padded FFT taken for each channel signal
- Magnitude responses overlaid





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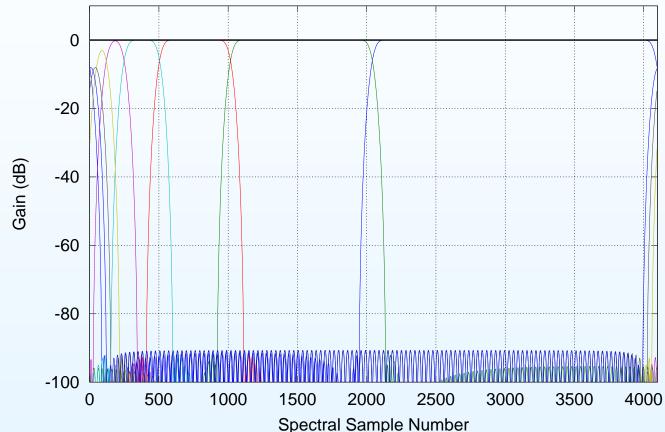
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Practical Octave Filter Bank

Interpolated Channel Signal Spectra



Improve channel-filter impulse responses:

Rectangularly windowed sinusoids

→ Chebyshev-windowed sinusoids





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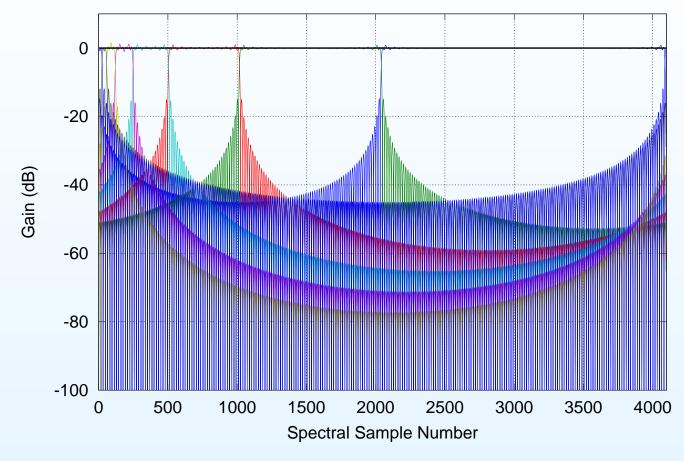
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Summary

Superposition of Channel Spectra after Critical Sampling

Interpolated Channel Signal Spectra after Aliased Reconstruction



- Each channel maximually downsampled
- Transition bands alias heavily
- Aliasing cancels in filter-bank sum





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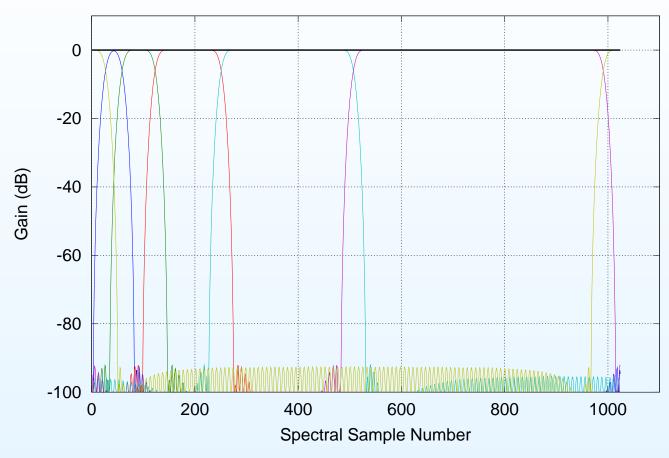
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IFFT Band Allocation Including Transition Bands

Channel Signal Spectra Interpolated by 4



As before but allocating wider overlapping IFFT bands:

- Passband plus transitions fit inside IFFT
- Passbands contiguous as before, but IFFTs overlap more





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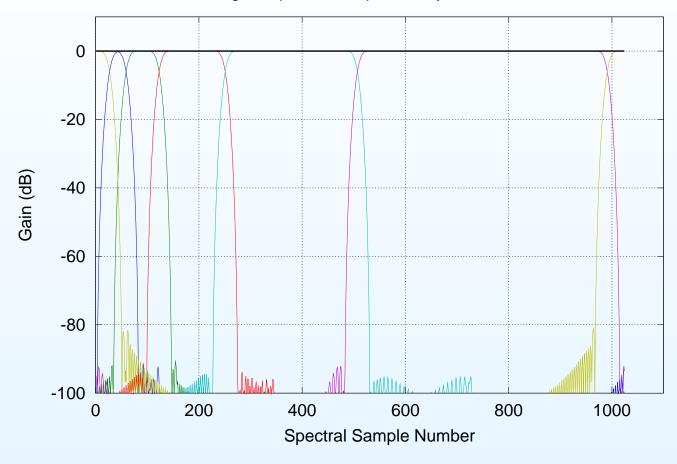
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Aliasing Suppression

Channel Signal Spectra Interpolated by 4 from Aliased Bands



Reconstruction after critical downsampling
Aliasing is reduced because now there is no aliasing of transition
bands





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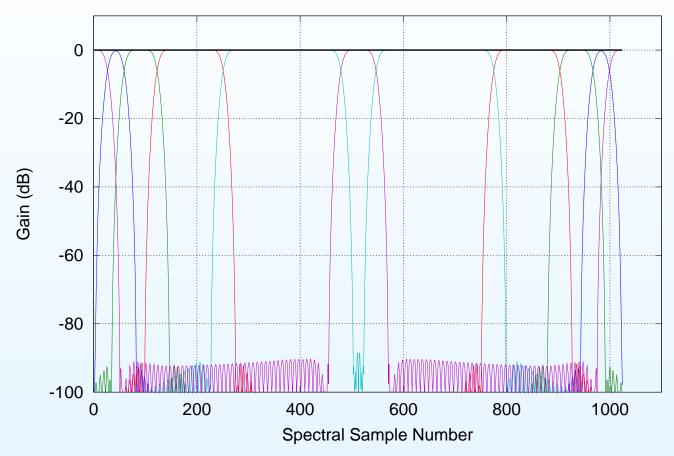
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Real Octave Filter Bank

Channel Signal Spectra Interpolated by 4



Approximate octave filter bank for real signals





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Notes on Audio FFT Filter Banks

- Arbitrary nonuniform spectral partitions and/or overlap-add decompositions are easily implemented, while preserving the FFT speed advantage
- Extension to time-varying nonuniform filter banks is straightforward
- Come see the poster this afternoon!





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Spectrally Matched Click Synthesis

While outside the 1-year limit, Matt Wright's poster this afternoon (4:30 pm) Spectrally Matched Click Synthesis is another work performed at least partially at CCRMA with JOS input.

- FIR filter design to achieve a minimum-duration "click" having a desired magnitude spectrum
- Applications:
 - Incremental attack strength modification
 - Continuous gradual "morphing" between an input sound and successively more impulsive/ percussive sounds





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Acoustically Transparent and Configurable Microphone Array





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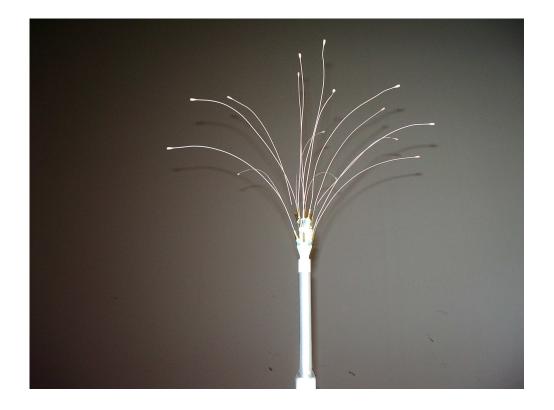
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- Mic Array
- Mic Array Paper

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- Adustable geometry (software calibrated)
- Sixteen microphones (Countryman B6 Omni Lavalier):
 - o 2 mm diameter capsules
 - 1 mm diameter flexible mounting wire
 - Acoustically transparent over most of the audio band





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Upcoming Paper

"A Configurable Microphone Array with Acoustically Transparent Omnidirectional Elements"

Jonathan Abel, Nicholas Bryan, Travis Skare, Patty Huang, Darius Mostowfi, Miriam Kolar, and Julius Smith

AES-2009, New York

Current Application:

Recording and modeling acoustic properties of underground galleries at pre-Inca archeological site Chavín de Huántar in Peru





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CCRMA/EE graduate student **Travis Skare** developed a *Faust* architecture file for Flash browser plugins:

- Faust generates C++ as usual
- Alchemy (by Adobe Labs) translates C++ to ActionScript
- Several Faust examples successfully compiled: pitch-shifter, freeverb, karplus, osc, multibandfilter
- Interesting points to note:
 - Flash version 10 needed for run-time sound processing
 - Delay from plugin controls to sound is about half a second
- Thanks to Google for allowing Travis to release his code as free software





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In summary, we took a quick look at some DAFx-Related Research involving JOS at CCRMA in 2008-2009:

- Spring Reverb Modeling Jonathan Abel et al. new propagation modes and calibration methods
- Digitizing Analog Circuits in Real Time David Yeh Automated K-Method for nonlinear analog circuits
- Coupled Strings Analysis and Synthesis Nelson Lee —
 Fourth-order modes for low partials, wavuide model for upper
 partials; new analysis techniques
- Haptic Virtual Instruments Ed Berdahl Real controllers (with force feedback) for virtual instruments





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Summary, continued

- Alias-Suppressed Virtual Analog Vesa Välimäki et al. differentiated higher-order polynomials suppress aliasing further than in the parabolic case (Välimäki 2005)
- Spectral Delay Filters Vesa Välimäki et al. "impulse response synthesis"
- Audio FFT Filter Banks JOS arbitrary nonuniform filter banks (spectral overlap-add decompositions) using overlapping IFFTs for each subband that include transition bands
- Microphone Array Jonathan Abel et al. Acoustically transparent, configurable, software-calibrated microphone array for sampling the 3D sound field
- Faust to Flash Plugins Travis Skare Tools for making Flash plugins from Faust source





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Further Details on Differentiated Polynomial Synthesis





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Further Details on Differentiated Polynomial Synthesis

- Max Smoothness
- Even-Odd Parts
- Even-Odd Properties
- Simplified Solution

Maximum Smoothness Problem Formulation

For maximum wraparound smoothness, compute a_n , $n \in [1, n-2]$, such that

$$f^{(k)}(-1) = f^{(k)}(1)$$

for
$$k = 0, 1, \dots, n - 1$$
.

- These equations yield an upper triangular system
- Triangular matrix equations are easily "back-solved"
- ullet Solution gives the *maximually flat coefficient*s for f(x)





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Even and Odd Polynomials

In general, f(x) is a sum of its even and odd parts:

$$f(x) = f_e(x) + f_o(x)$$

where

$$f_e(-x) = f_e(x) \stackrel{\triangle}{=} \frac{f(x) + f(-x)}{2}$$

$$-f_o(-x) = f_o(x) \stackrel{\Delta}{=} \frac{f(x) - f(-x)}{2}$$

• Even part $f_e(x)$ contains all *even powers* of x:

$$f_e(x) = \dots + a_4 x^4 + a_2 x^2 + a_0$$

• Odd part $f_o(x)$ contains all *odd powers* of x:

$$f_o(x) = \dots + a_5 x^5 + a_3 x^3 + a_1 x$$





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- Simplified Solution

Solution Properties of Even and Odd Polynomials

We have

$$f(x) = f_e(x) + f_o(x)$$

where

$$f_e(x) = \frac{f(x) + f(-x)}{2}$$

$$f_o(x) = \frac{f(x) - f(-x)}{2}$$

- Note that $f_e(-1) = f_e(1) \Rightarrow$ smoothness constraint satisfied spontaneously by even part
- Since $f_o(-1) = -f_o(1)$, we must have $f_o(1) = 0$ \Rightarrow sum of f_o coefficients must be zero in odd part





Spring Reverb Models

Virtual Analog Circuits

Acoustic Guitar Models

Haptic Instruments

New Oscillators

Spectral Delay Filters

Audio FFT Filter Banks

Microphone Array

Faust to Flash Plugins

Summary

Further Details on Differentiated Polynomial Synthesis

- Max Smoothness
- Even-Odd Parts
- Even-Odd Properties
- Simplified Solution

Simplified Maximum Smoothness Solution

- If f(x) is an odd-order polynomial satisfying $f^{(k)}(-1)=f^{(k)}(1)$ for $k=0,1,\ldots,n-1$, then it continues to satisfy those constraints when its even part is replaced by zero
- Similarly, the odd part of an even-order polynomial f(x) may be set to zero without affecting its wraparound smoothness
- Thus, without loss of generality, the starting polynomial f(x) may be taken as even or odd, according its order
- The derivative of an even polynomial is odd, and vice versa
- Every other polynomial derivative has the sum-to-zero constraint
- Upper triangular system is reduced by about half

